

July 30 Meeting – Points to discuss – Proposed by Anish Jantrania

Point #1: Virginia Tech Research Summary

Research Period – From November 1999 to June 2001 (22 Months)

Septic Tank Effluent (STE) versus Recirculating Media Filter (RMF) Effluent – Effects of Loading Rate, Soil Depth, and Fecal Coliform; Column study and Field study.

**COLUMN STUDY**

| RMF + Soil FC >200 counts   |     |     |     | RMF Sample Size   |     |     |     | RMF Sampling Attempts |    |    |    |
|-----------------------------|-----|-----|-----|---|-----|-----|-----|-----------------------|----|----|----|
|                             | 2x  | 3x  | 5x  |   | 2x  | 3x  | 5x  |                       | 2x | 3x | 5x |
| 15                          | 6   |     | 9   | 15  | 16  |     | 26  | 15                    | 34 |    | 51 |
| 30                          | 11  | 7   | 13  | 30  | 27  | 26  | 33  | 30                    | 51 | 34 | 51 |
| 45                          | 9   |     | 12  | 45  | 42  |     | 27  | 45                    | 51 |    | 51 |
| STE + Soil FC >200 counts   |     |     |     | STE Sample Size   |     |     |     | STE Sampling Attempts |    |    |    |
|                             | 1x  |     |     |   | 1x  |     |     |                       | 1x |    |    |
| 45                          | 23  |     |     | 45  | 27  |     |     | 45                    | 51 |    |    |
| RMF % FC >200 counts        |     |     |     | Overall Probability for FC >200 w/ RMF ={(samples/attempts)*(hits/samples)} |     |     |     |                       |    |    |    |
|                             | 2x  | 3x  | 5x  |   | 2x  | 3x  | 5x  |                       | 2x | 3x | 5x |
| 15                          | 38% |     | 35% | 15  | 18% |     | 18% |                       |    |    |    |
| 30                          | 41% | 27% | 39% | 30  | 22% | 21% | 25% |                       |    |    |    |
| 45                          | 21% |     | 44% | 45  | 18% |     | 24% |                       |    |    |    |
| STE + Soil % FC >200 counts |     |     |     | Overall Probability for FC >200 w/ STE                                      |     |     |     |                       |    |    |    |
|                             | 1x  |     |     |   | 1x  |     |     |                       | 1x |    |    |
| 45                          | 85% |     |     | 45  | 45% |     |     |                       |    |    |    |
| GeoMean RMF+Soil            |     |     |     | Excluding 0 and missing values  |     |     |     |                       |    |    |    |
|                             | 2x  | 3x  | 5x  |   |     |     |     |                       |    |    |    |
| 15                          | 220 |     | 91  |   |     |     |     |                       |    |    |    |
| 30                          | 120 | 148 | 121 |   |     |     |     |                       |    |    |    |
| 45                          | 82  |     | 341 |   |     |     |     |                       |    |    |    |
| GeoMean STE+Soil            |     |     |     | Excluding 0 and missing values  |     |     |     |                       |    |    |    |
|                             | 1x  |     |     |   |     |     |     |                       |    |    |    |
| 45                          | 745 |     |     |   |     |     |     |                       |    |    |    |

**FIELD STUDY**

| RMF Sample Size |          |                   |     |
|-----------------|----------|-------------------|-----|
|                 | 1x       | 2x                | 5x  |
| 15              | 13       | 11                | 8   |
| 30              | 14       | 11                | 12  |
| 45              | Not Done | 7                 | 20  |
|                 |          |                   | 96  |
| STE Sample Size |          |                   |     |
|                 | 1x       |                   |     |
| 45              | 29       |                   | 29  |
|                 |          |                   |     |
|                 |          | Total Samples =   | 125 |
|                 |          | Samples >0 =      | 2   |
|                 |          | 1 sample for STE  |     |
|                 |          | 1 sample for RMFE |     |
|                 |          | STE+45cm1x=       | 150 |
|                 |          | RMFE+45cm5x=      | 1   |

Photo of Soil Column at the end of the study period



Photo from Prof. Ray Reneau, Virginia Tech.

Pictures of Drip System from two sites in Virginia

Drip system dispersing STE



Drip system dispersing Sand Filter Effluent



Photos taken by Anish Jantrania with Lots of help from Bob Mayer and Tom Ashton.

**THIS DOES NOT MEAN THAT SEPTIC TANK EFFLUENT DISPERSAL IN SOIL IS A BAD IDEA! WE JUST NEED TO CONSIDER BETTER LOADING RATE NUMBERS FOR STE!**

STE Effluent Drain Field after some years of use Real World Pictures



Source: Friends from GA (Gravity System)



Source: Friends from WA (Pressure System)

Point #2 Defining Prescriptive Drain Field Design For Achieving Performance Standards

**Approach #1 Loading Rate and Horizontal Setbacks**

- Hydraulic loading rate cannot be greater than allowable organic loading rate;
- Organic loading rate must be decreased for sites where depth of aerobic soil is less than 18”
- Hydraulic loading rate cannot be greater than some fraction of Ksat for Ksat values >1 cm/day

Loading Rate Adjustment for Treatment (TS1, TS2, TS3, and TS4 & Available Vertical Standoff (>18”, 12”-18”, 6”-12”, and <6”)

Following Arizona Formula for Treatment Credits & Anish’s Proposal for Loading Rate Adjustment for Available Vertical Standoff, following adjustment values are proposed:

|                   |         |     |  | % Increase in LR     |      |      |      |     |
|-------------------|---------|-----|--|----------------------|------|------|------|-----|
|                   |         |     |  |                      | 75%  | 150% | 300% |     |
|                   |         |     |  | TS1                  | TS2  | TS3  | TS4  |     |
| % Reduction in LR | 0.00150 | IC1 |  | 1.00                 | 1.75 | 2.50 | 4.00 |     |
| 50%               | 0.00075 | IC2 |  | 0.50                 | 1.25 | 2.00 | 3.50 |     |
| 70%               | 0.00045 | IC3 |  | 0.30                 | 1.05 | 1.80 | 3.30 |     |
| 90%               | 0.00015 | IC4 |  | 0.10                 | 0.85 | 1.60 | 3.10 |     |
|                   |         |     |  |                      |      |      |      |     |
|                   |         |     |  | BOD mg/l =           | 300  | 30   | 15   | 3   |
|                   |         |     |  | % Reduction in BOD = |      | 90%  | 95%  | 99% |

Applying Safety Factors to Measured or Estimated Ksat (Saturated Hydraulic Conductivity) Values for Calculating Loading Rates

| Ksat Class      | Typical range cm/day | % of Ksat Allowed for TBA |
|-----------------|----------------------|---------------------------|
| Very High       | ≥ 864                | 5%                        |
| High            | 86.4 - 864           | 10% - 5%                  |
| Moderately High | 8.64 - 86.4          | 15% - 10%                 |
| Moderately Low  | 0.864 - 8.64         | 20% - 15%                 |
| Low             | 0.086 - 0.864        | 25% - 20%                 |
| Very Low        | < 0.086              | 25%                       |

MINIMUM ALLOWABLE TRENCH BOTTOM AREA LOADING RATES FOR MEASURED OR ESTIMATED KSAT <1 CM/DAY (IMPERMEABLE SOIL)

TS1 = 0.01 GPD/SQFT

TS2 = 0.06 GPD/SQFT

TS3 = 0.12 GPD/SQFT

TS4 = 0.60 GPDSQFT (Demo projects in VA support this number!)

USE THE LOADING RATE CALCULATOR DEVELOPED BY ANISH JANTRANIA FOR DETERMING TRENCH BOTTOM AREA LOADING RATE FOR YOUR SITE.

## Horizontal Setback Adjustment Proposal for Treatment & Management

|   |                   |     | EPA Management Model 1, 2, 3 | EPA Management Model 4, 5 |  |  |
|---|-------------------|-----|------------------------------|---------------------------|--|--|
| TS =  | <b>TS4</b>        | TS2 | 10%                          | 30%                       |  |  |
| Management =  | <b>Model 4, 5</b> | TS3 | 15%                          | 50%                       |  |  |
|   |                   | TS4 | 20%                          | 70%                       |  |  |
| Reduction Factor =  | <b>0.70</b>       |     |                              |                           |  |  |
| Example: Distance from Edge of Effluent System to Property Lines            |                   |     |                              |                           |  |  |
| for TS4 & Management Model 4, 5 = $100 * (1 - 0.7) = 30$ feet               |                   |     |                              |                           |  |  |
| <b>NOTE: Management Model 4, 5 are STRONGLY RECOMMENDED for TS3 and TS4</b> |                   |     |                              |                           |  |  |

### Horizontal Setback Chart for TS4 and Management Model 4, 5:

| Structure or Topographic Features  | Minimum Distance (Ft) from Edges of Effluent Disposal System to Features |                      |
|--|--|----------------------|
|  | FOR TS1 and Management 1, 2, 3   | For Higher Treatment |
| Property Lines Up Gradient (Slope>5%)  | 10   | 5                    |
| Property Lines Down Gradient (Slope>5%)  | <b>100</b>   | 30                   |
| Building Foundations   | 10   | 5                    |
| Basements  | 20   | 10                   |
| Active Groundwater Water Wells   |  |                      |
| Class IIIA or IIIB   | 50   | 15                   |
| Class IIIC or IV   | 100  | 30                   |
| Abandon Ground Water Wells   |  |                      |
| Class IIIA or IIIB   | 25   | 10                   |
| Class IIIC or IV   | 50   | 15                   |
| Cisterns (Applicable only when bottom elevation of cistern is lower than ground surface) | 100  | 30                   |
| Shellfish Waters   | 70   | 25                   |
| Natural Lakes & Impounded Waters   | 50   | 15                   |
| Streams  | 50   | 15                   |
| Developed Springs (Applicable only when the spring is down slope)                        | 200  | 60                   |
| Drainage Ditches when Ditch Bottoms above Seasonal Water Table                           | 10   | 5                    |
| Drainage Ditches when Ditch Bottom below Seasonal  | 70   | 25                   |
| Water Table Depressor System   | 70   | 25                   |
| Lateral Ground Water Movement Interceptor  | 70   | 25                   |
| Low Point of Sink Holes  | 100  | 30                   |
| Utility Lines  | 10   | 5                    |

Use the Spreadsheet to determine values for different TS and Management.

## Approach #2 Flow-Area-Index and Horizontal Setbacks

When the designer (Professional Engineer) wants to deviate from the Loading Rate Calculator then the Flow-Area-Index (Ratio of Flow to Project Area – FAI) must meet the following proposed inch/year values:

| <b>Suggested FAI:</b>          |                              |                               |                               |
|--------------------------------|------------------------------|-------------------------------|-------------------------------|
|                                | Management Model Proposed    |                               |                               |
| Treatment Levels               | EPA Management Model 1, 2, 3 | EPA Management Model 4, 5 Pvt | EPA Management Model 4, 5 Pub |
| TS1 (Septic Tank)              | <b>0.6</b>                   | <b>1.2</b>                    | <b>1.5</b>                    |
| TS2 (Secondary)                | <b>1.2</b>                   | <b>4.0</b>                    | <b>5.0</b>                    |
| TS3 (Secondary + Disinfection) | <b>2.4</b>                   | <b>5.0</b>                    | <b>6.0</b>                    |
| TS4 (TS3 + Nutrient Reduction) | <b>3.0</b>                   | <b>6.0</b>                    | <b>&gt;6.0</b>                |

$$\text{FAI (inch/year)} = 0.01344x \frac{\text{GPD}}{\text{Acres}}$$

Where *GPD* = Proposed Design Flow and *Acres* = Project area in Acres.

Management models 4 & 5 are strongly recommended for TS3 and TS4.

With FAI and Horizontal Setbacks requirements met, the designer (Professional Engineer) and the Management Entity (RME/Utility) can select any loading rate for drain field as long as hydraulic performance requirements (no sewage back and no surfacing) are assured.

The proposed values of FAI ensure that the pollution load impact from a proposed onsite system will be contained within the property boundaries, thus ensuring no adverse cumulative impact on environmental quality from multiple onsite systems within any watershed boundary or political boundary.

An onsite system design is only 1/3<sup>rd</sup> of the total equation. The system must be installed according to the design (assuming that an installer can install the system that is designed), and then the system must be managed (operated and maintained) based on the design specifications in order to get the system to perform.

Performance quality = Design quality + Installation quality + Management quality.

Also, cumulative impact of the systems operated within a drainage basin must be accounted for in order to assure no adverse impact on environmental quality. This means that all the permitted systems must be able to “assimilate” waste load within the property on which the waste is generated. The suggested FAI chart is expected to achieve this goal and thus proposed for starting the performance based regulatory program in VA.